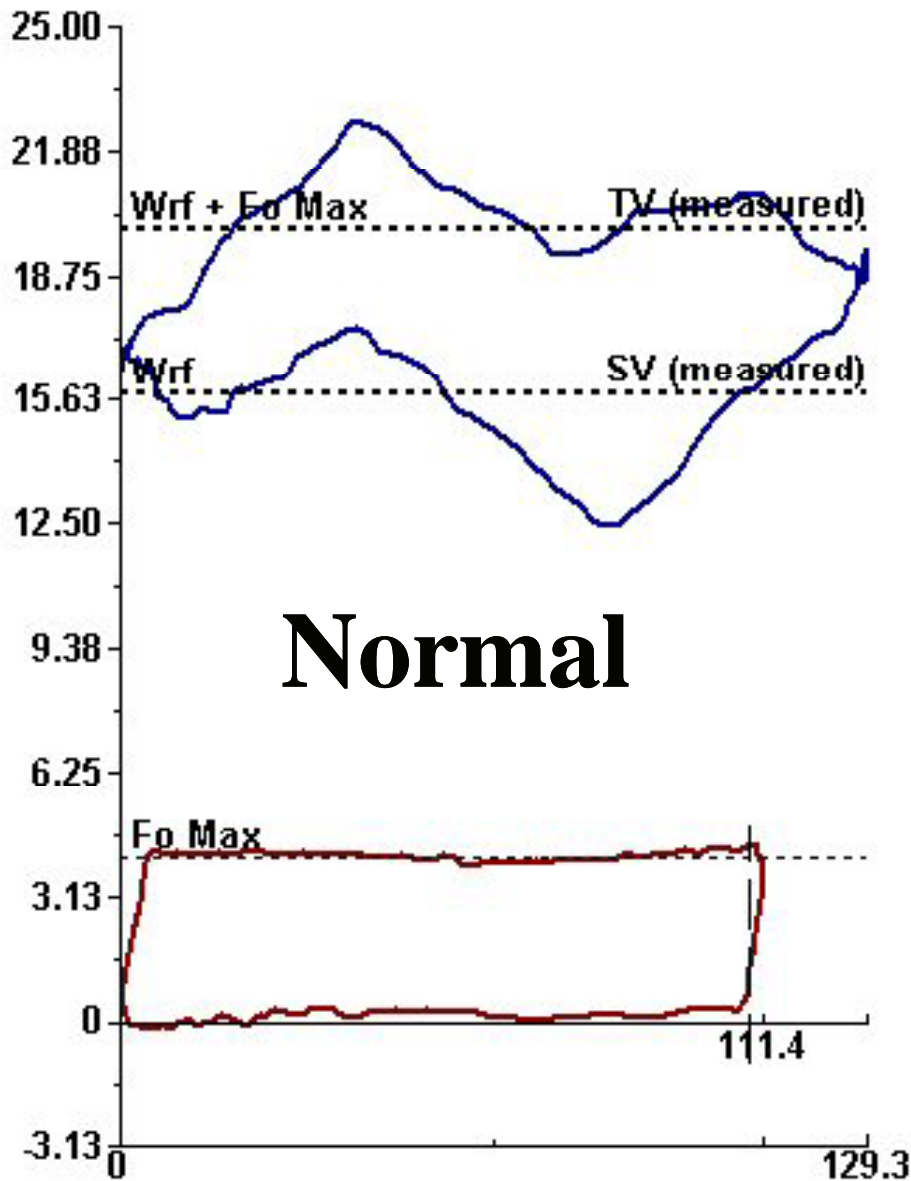


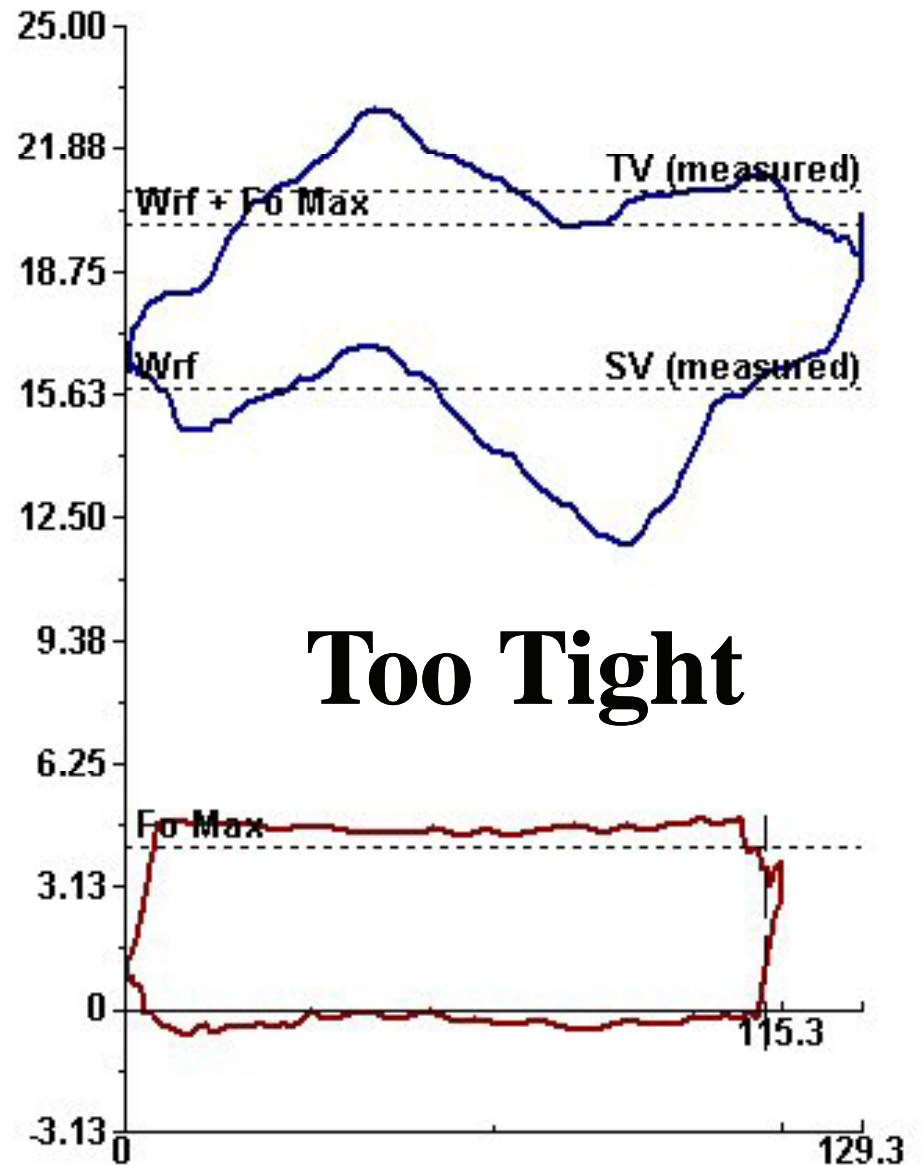
Artificial Lift Analyst Function:

- 1. Goal is to answer the WELL PERFORMANCE QUESTIONS**
- 2. Time Requirement is about 45 minutes per well.**
- 3. Analyze collected data at the well.**
- 4. Make recommendations to fix any problems discovered.**
- 5. Record work necessary to fix problem as notes in the comments text box.**
- 6. When recommended changes completed, new data should be collected once the well stabilized**
- 7. Notice if well performance changed as planned.**
- 8. Follow-up on recommendations to learn from successes and failures**
- 9. Role changes from a data collector to a knowledgeable well analyst and problem solver.**

Abnormal Loads – Tight Stuffing Box

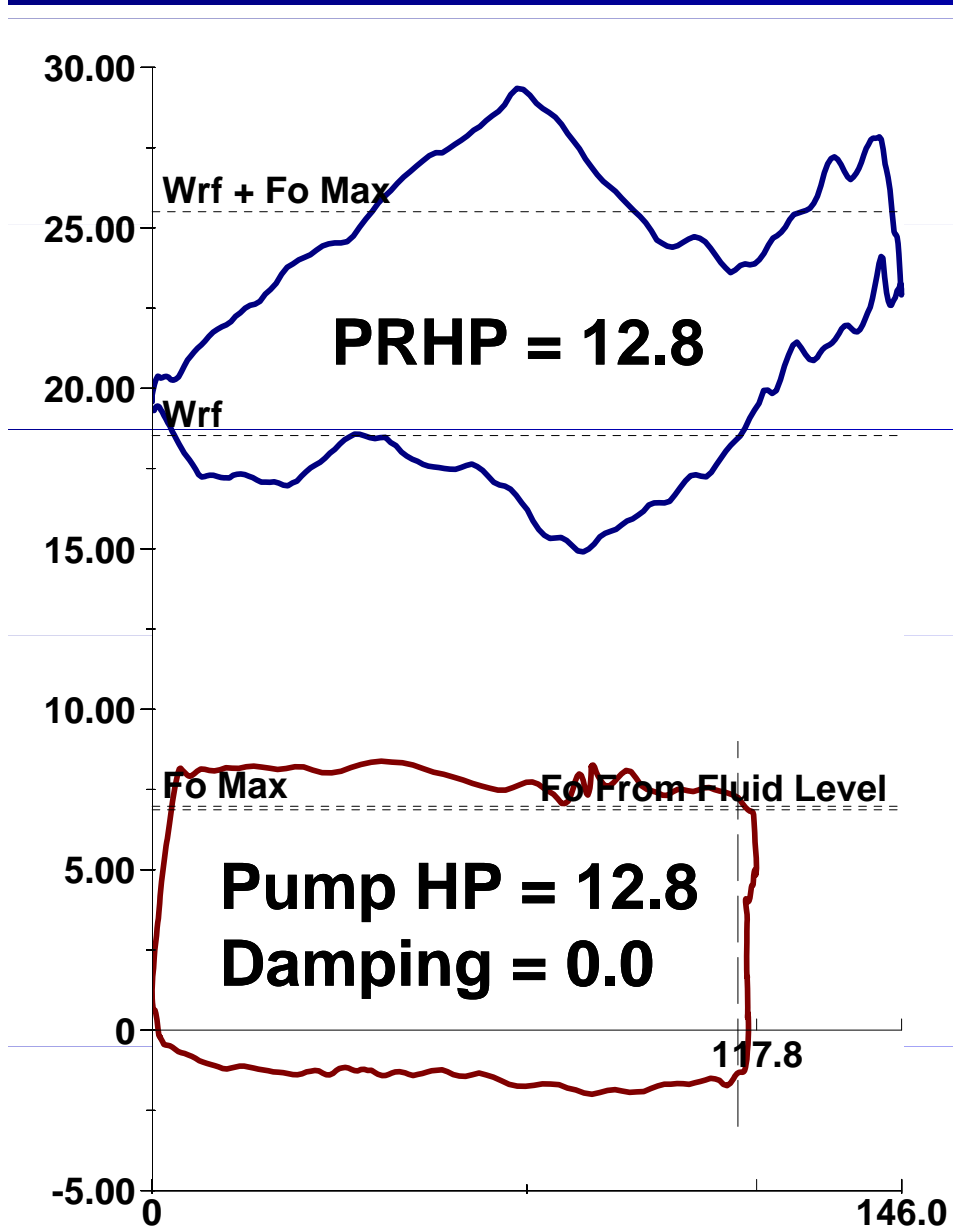


Normal



Too Tight

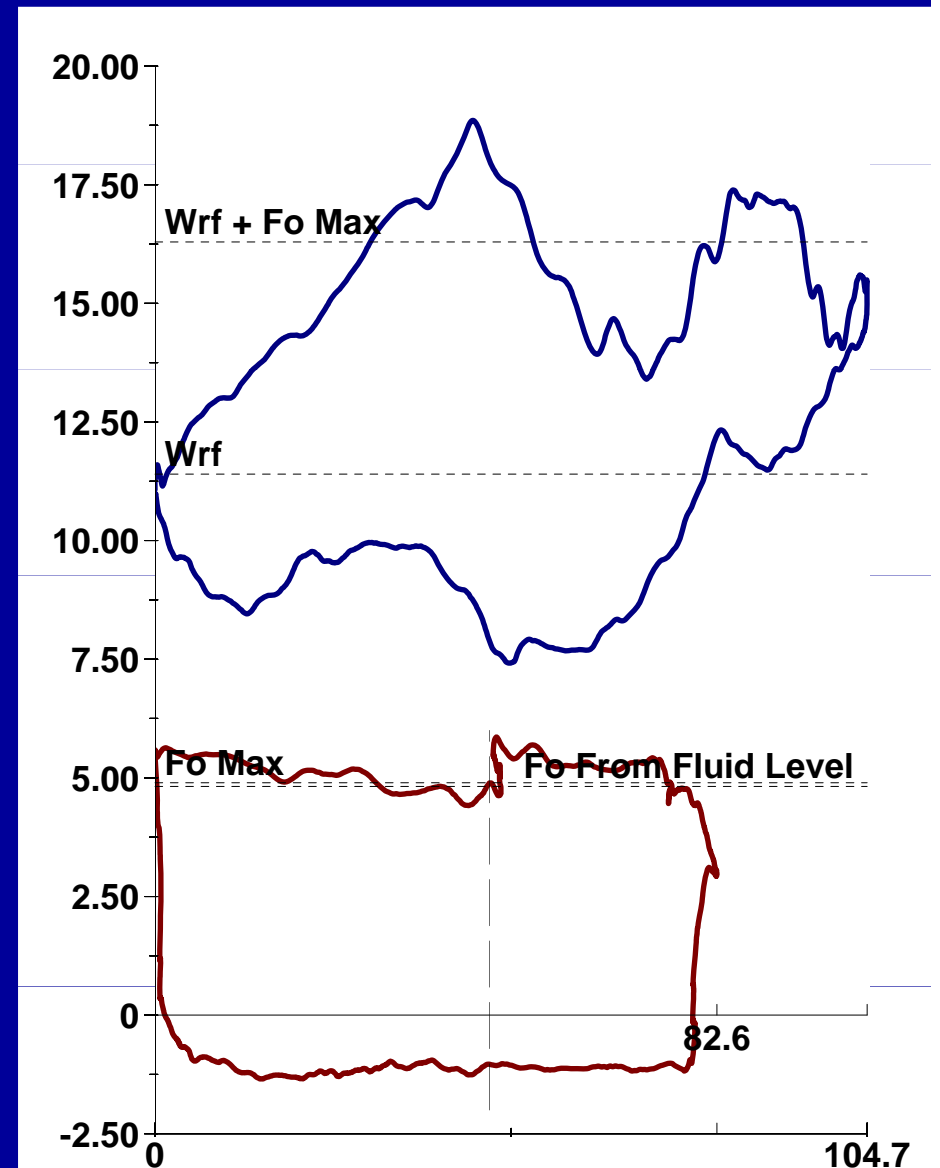
Damping for Pump Set in Horizontal



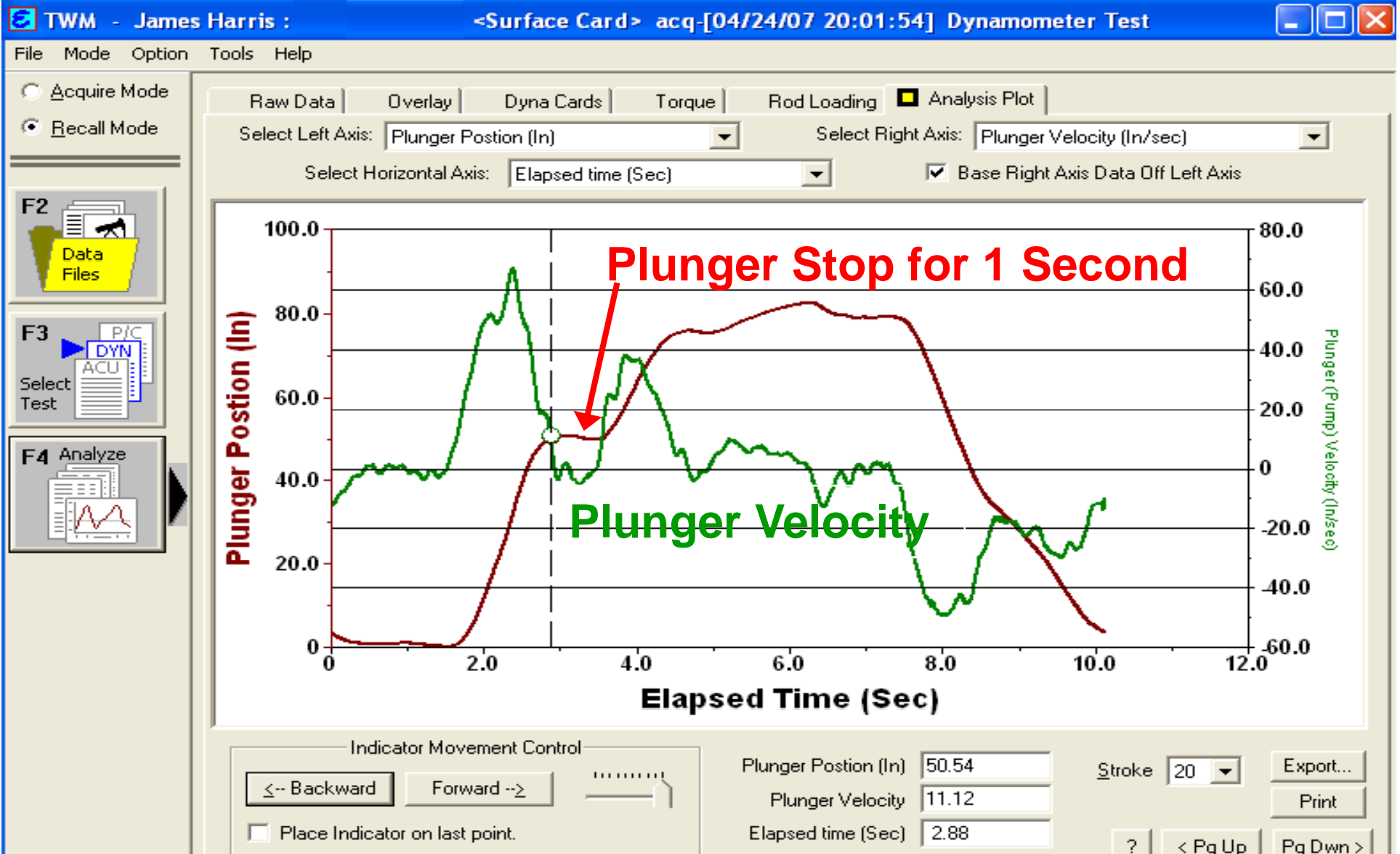
1. Polish Rod HP Minus Damping Equals Pump HP.
2. Polish Rod Horsepower less frictional horsepower equals the hydraulic horsepower, and represents work being done at the pump.

Dynamometer Cards

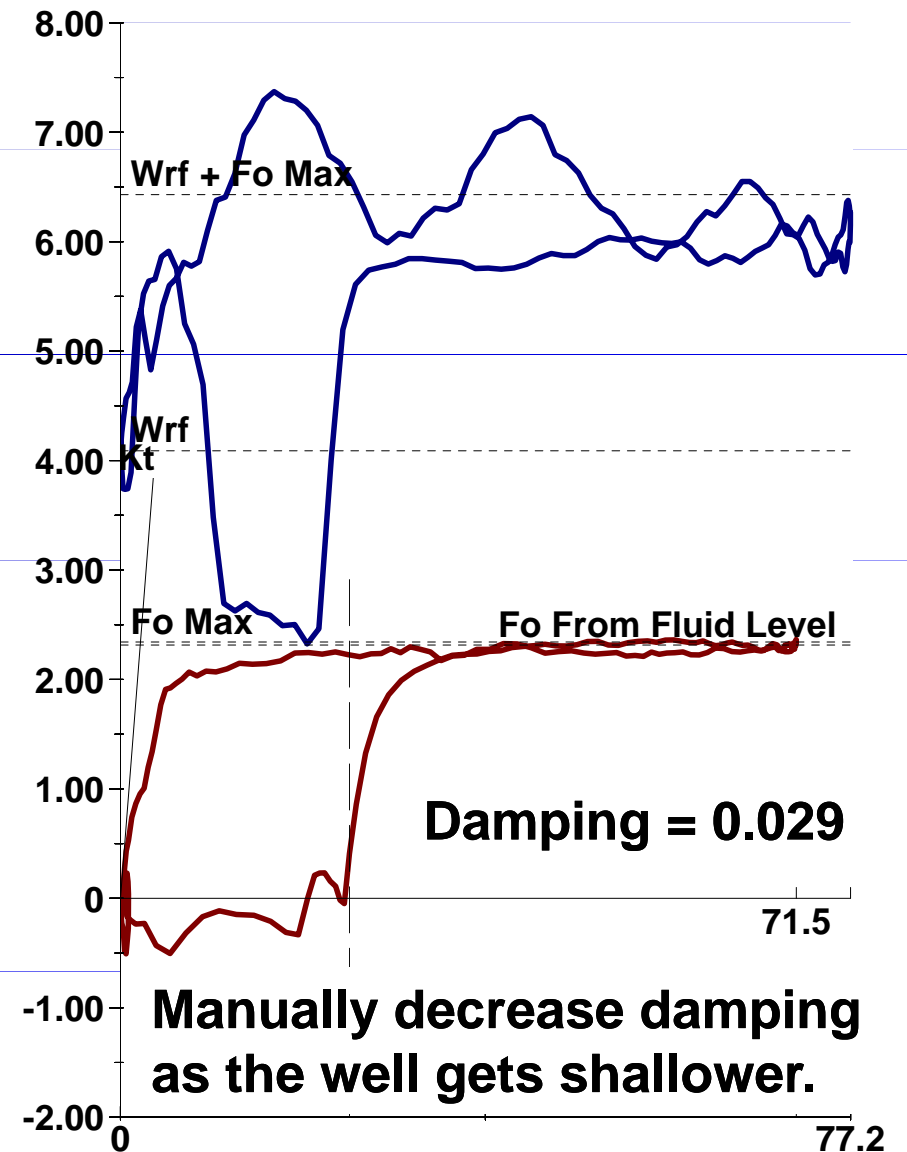
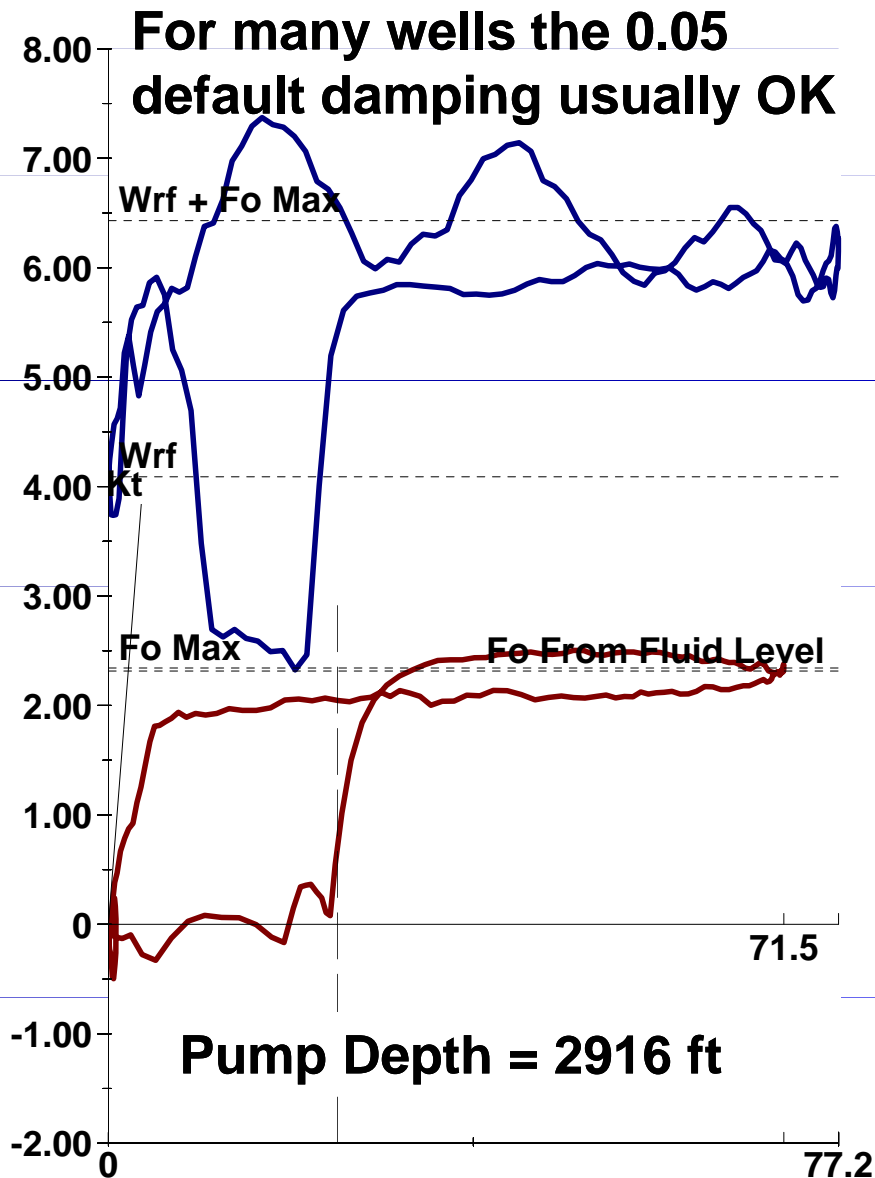
- 1) Diagnostic dynamometer surface cards used for Diagnosing Sucker Rod Pumping Systems.
- 2) Pump dynamometer card is to identify and analyze downhole problems.
- 3) Spike load at 49.5 inches on Stroke #20 shows when the plunger stopped on the upstroke. Unusual shape occurs over a 1 second time period and represents 1850 lb load increase required to overcome the downhole friction.



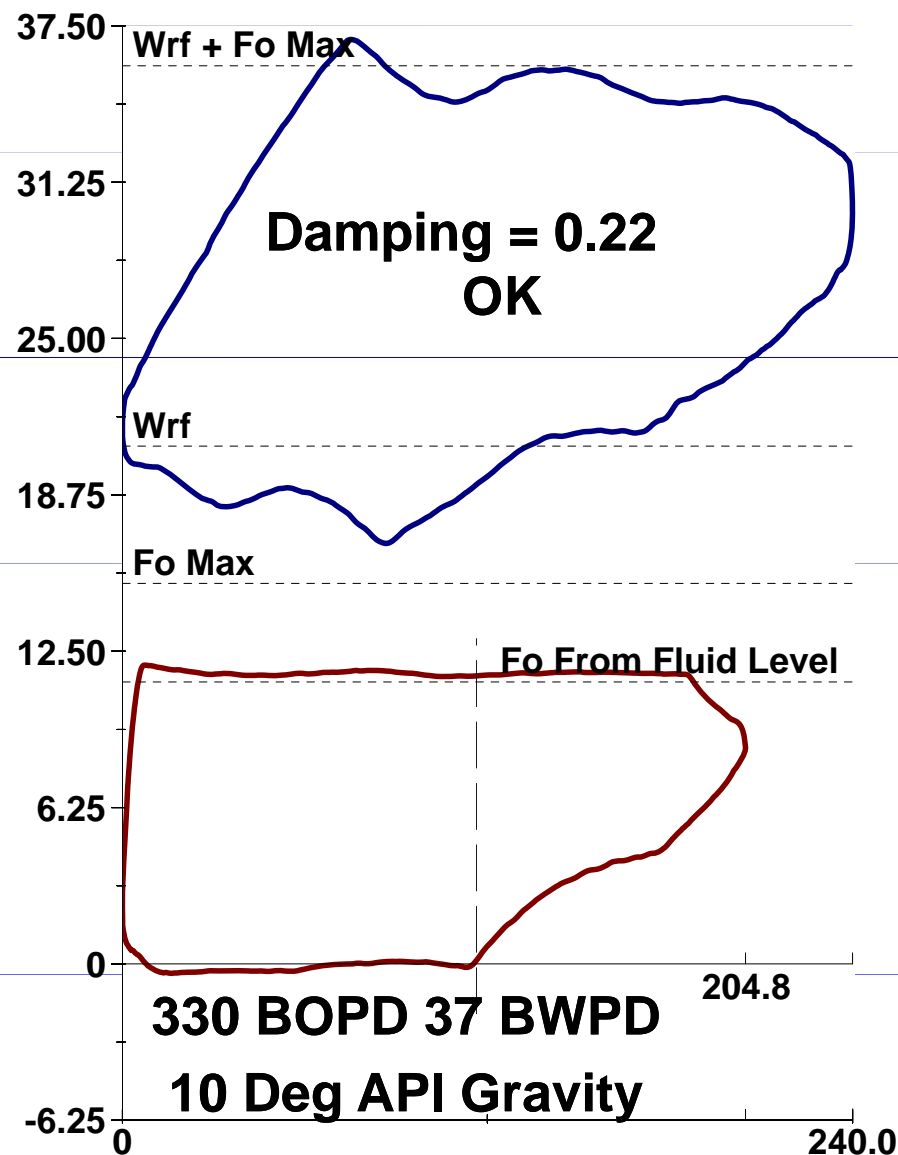
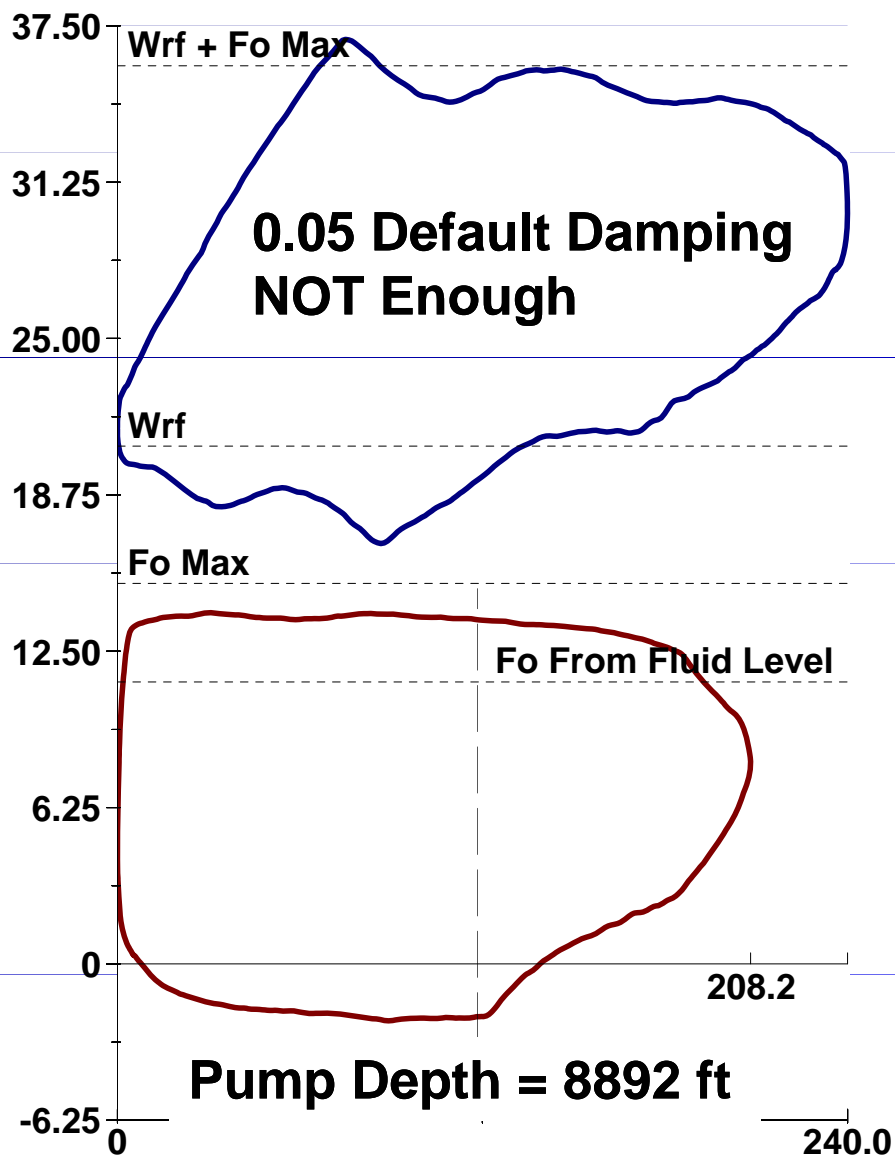
15 inches of Surface Stroke (73-88 inches on Upstroke) Lost to Rod Stretch in-order to apply Force to overcome Sudden 1850 lbs of Unknown Friction on Rods and Plunger



Damping Coefficients for Shallow Wells are usually 0.01/1000 foot of Pump Depth

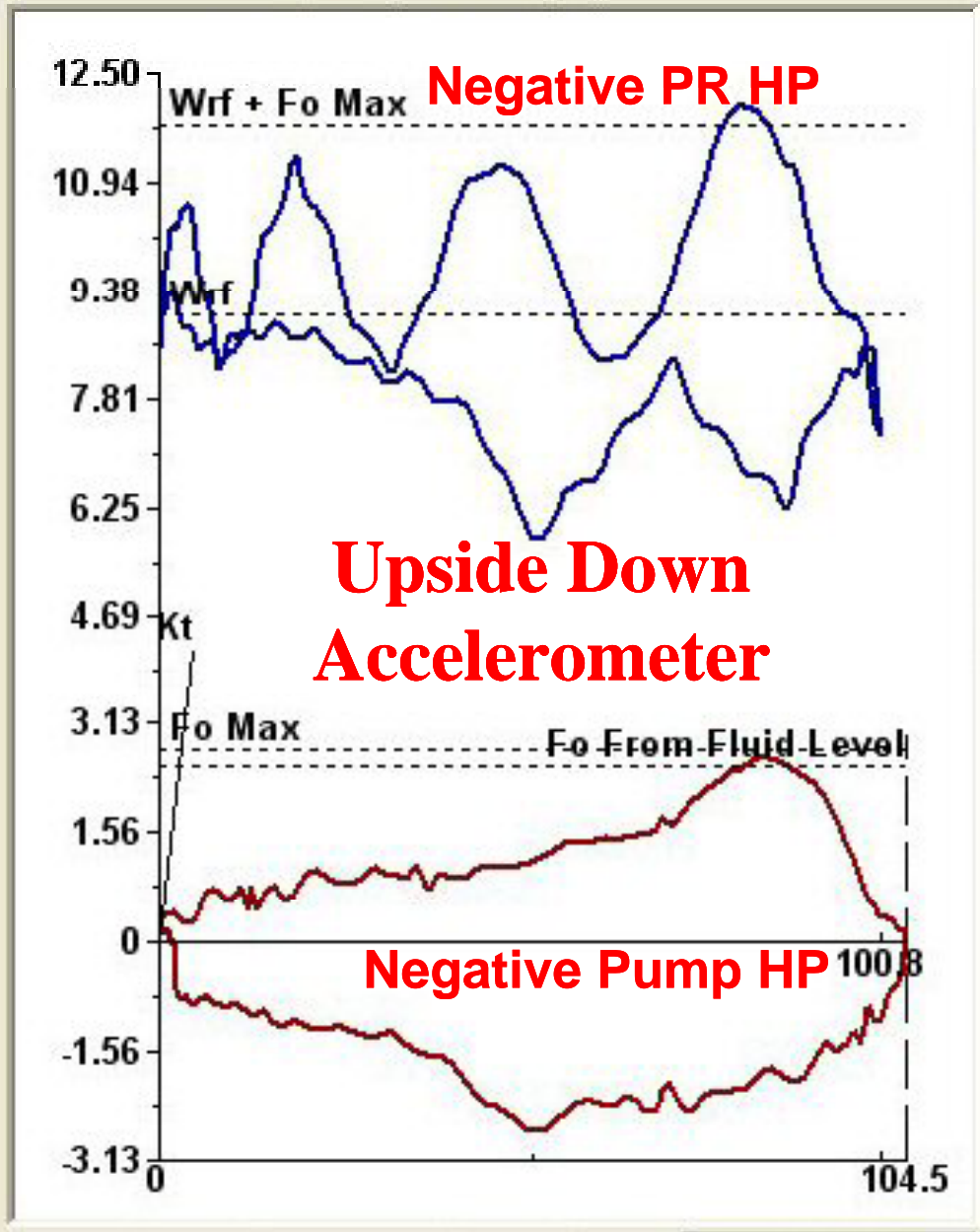


Damping Coefficients for Viscous Crude



Load(K-Lbs) vs Position (in)

HT 797
 PPRL 12033 PPUMPL 2645
 MPRL 5820 MPUMPL -2683



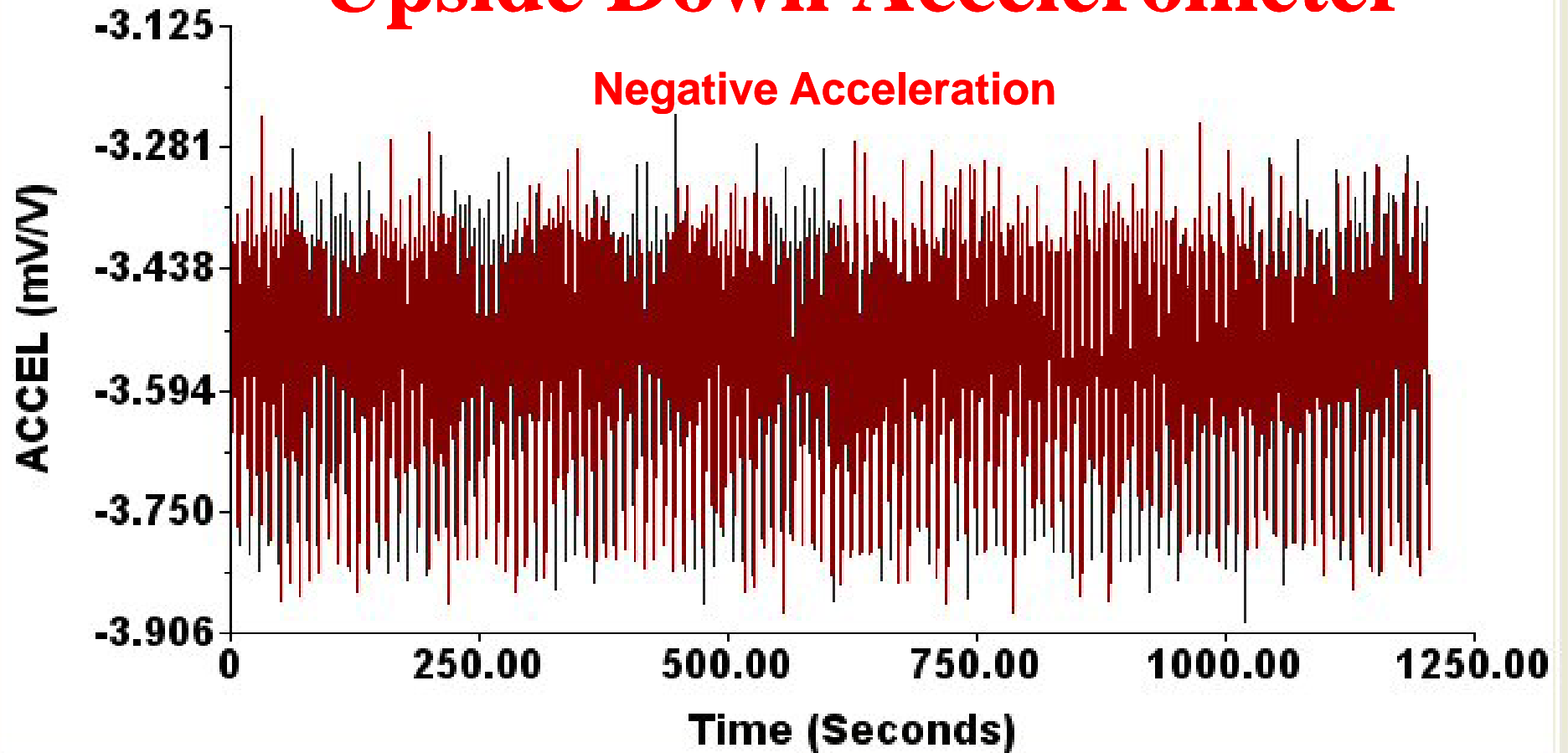
Calculated Fluid Load Max 2744 lb
 Polished Rod Power -3.5 HP
 Polished Rod / Motor Eff. 24.7 %
 Strokes Per Minute 6.23
 Pump Card HP -4.8 HP
 Pump / Motor Eff. -34.2 %
 Pump Displacement 118.6 BBL/D
 Pump Intake Pressure... 4019.1 psi (g)
 Damp Up 0.05
 Damp Down 0.05
 Tubing Head Pressure 77.5 psi (g)
 Effective Plunger Stroke
 100.00 % 104.5 in
 Stroke 68

Raw Data | Overlay | Dyna Cards | Torque | Rod Loading | Analysis Plot

Select Graph: Acceleration

Upside Down Accelerometer

Negative Acceleration



Show data in Engineering Units (e.g., lbs, in, etc...)

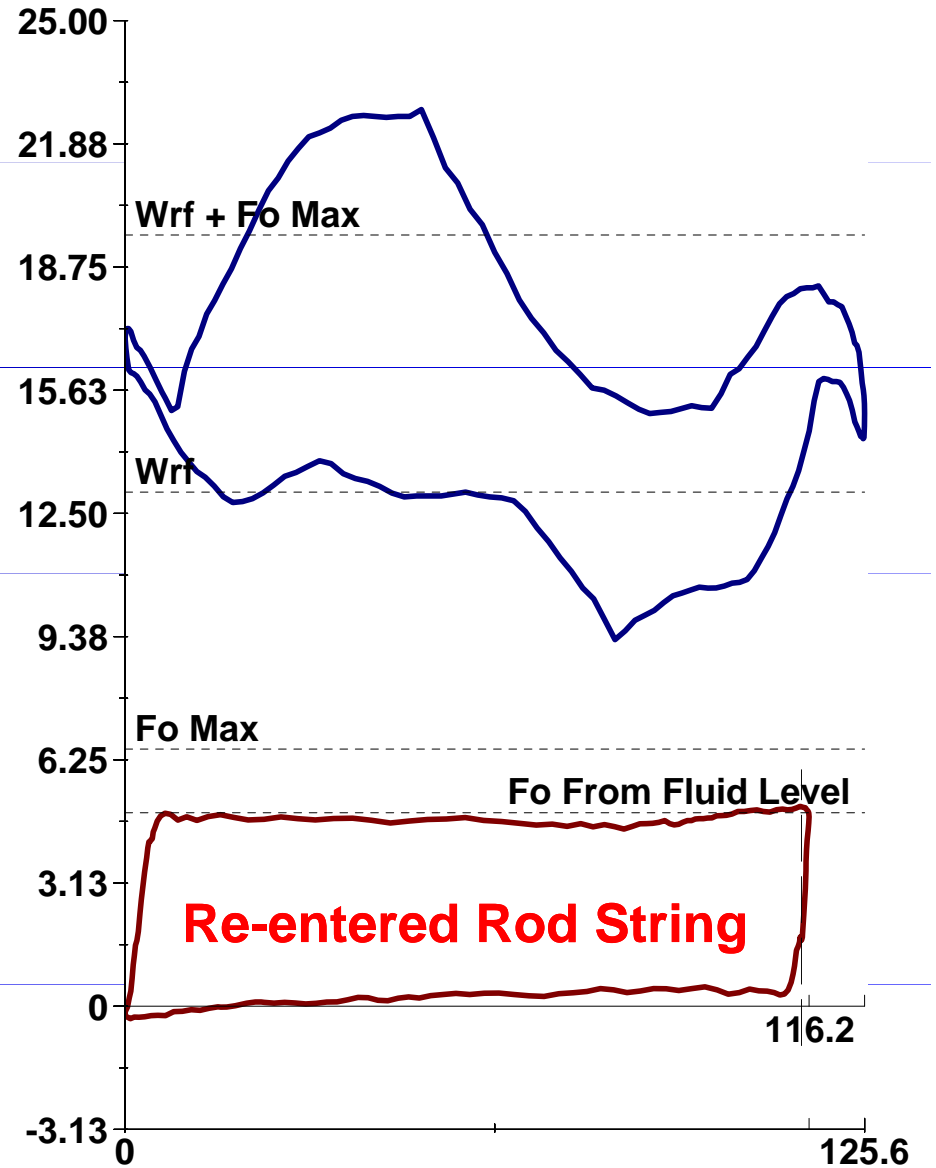
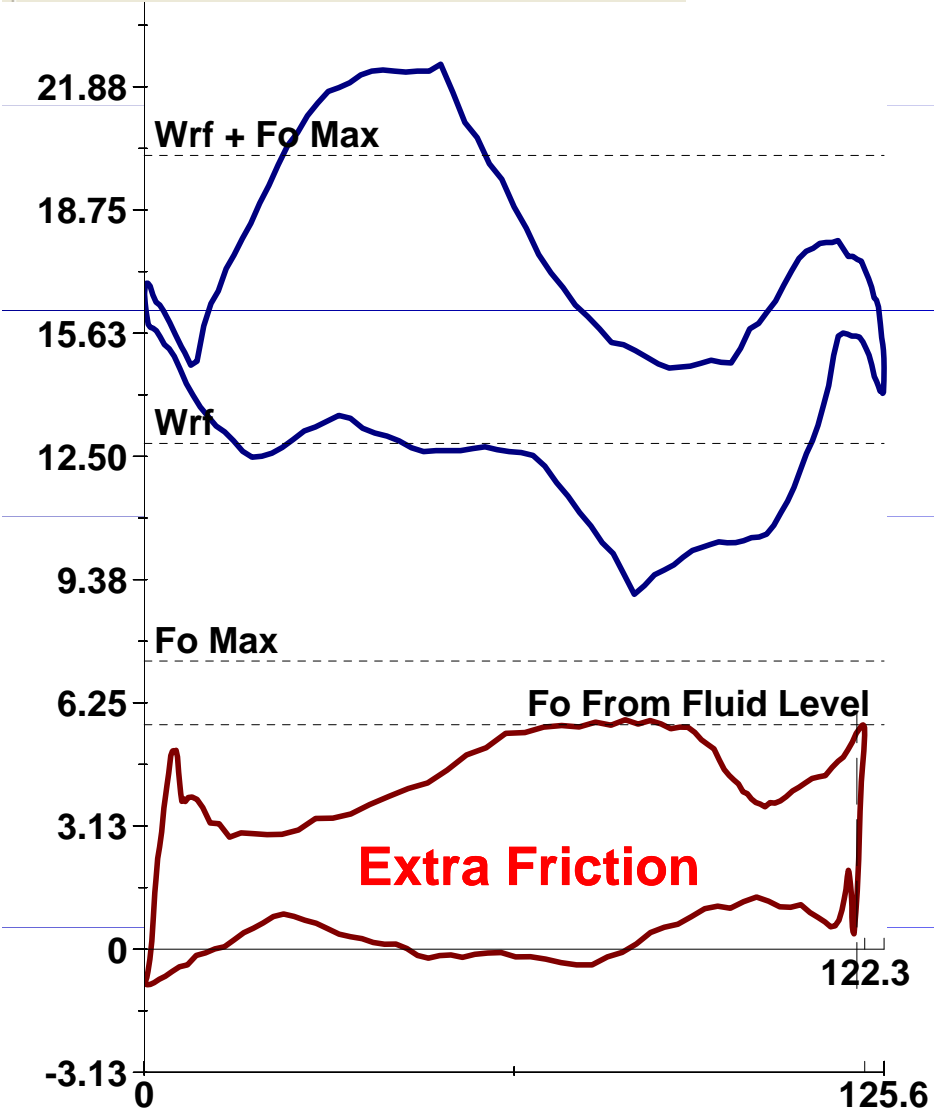
?

< Pg Up

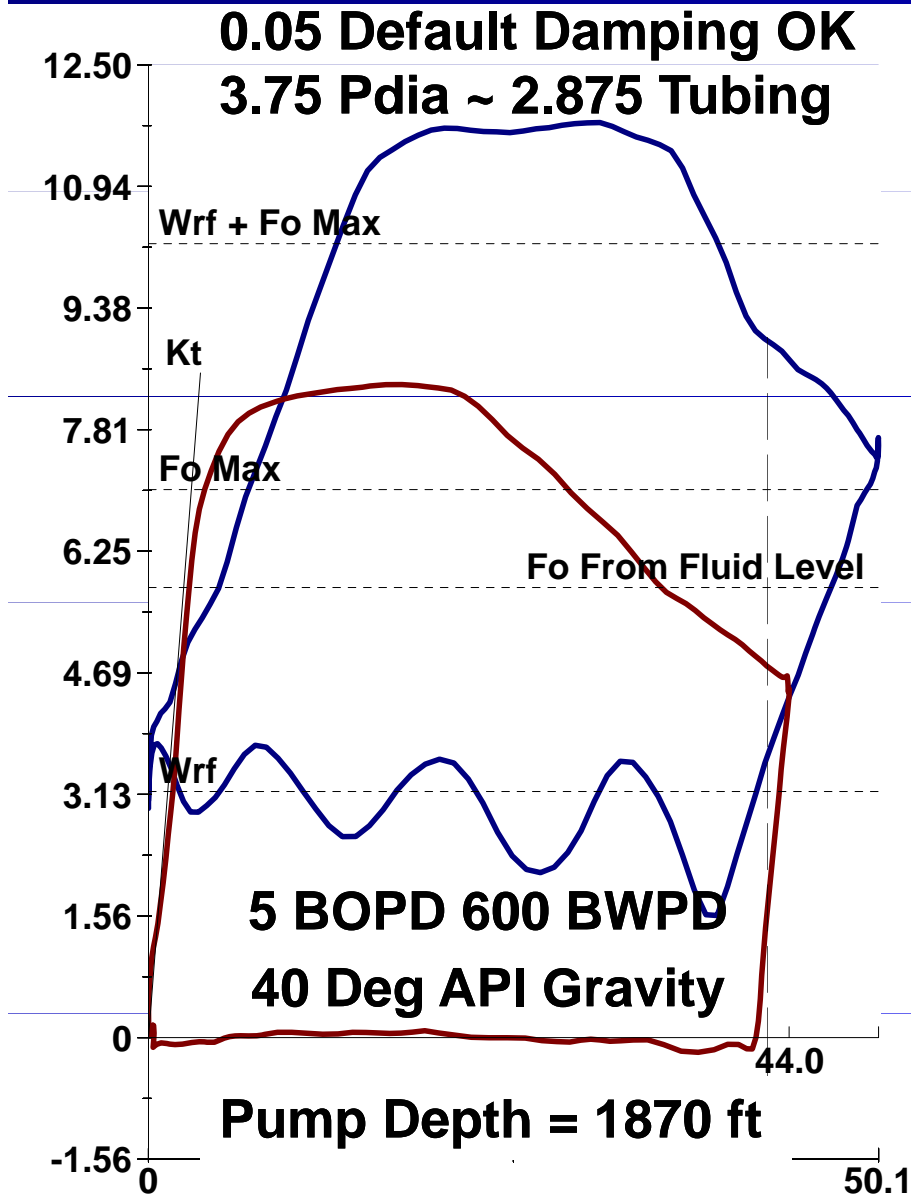
Pg Dwn >

Need to Change Damping?

	Top Taper	Taper 2	Taper 3
Rod Type	D	D	KD
Length	2275.00	2200.00	2150.00
Diameter	0.750	0.875	1.000
Weight	3693.3	4866.4	6218.2



Damping Coefficients for Bottled up Pump

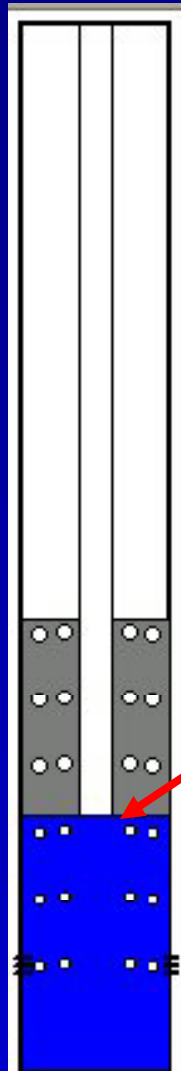


1. Pump card should fall below the FoMax line and rest on the Zero load line.
2. Restricted Discharge Area Resist Flow of Fluid out of the Pump (for example if the plunger area is greater than the area between the tubing and rods, then the pump must apply extra pressure to the fluid above the required discharge pressure)
3. Extra pressure inside pump barrel results in additional fluid load on the rods from the plunger; then the pump card Fo line can go above FoMax.

Damping Coefficients Impact PIP

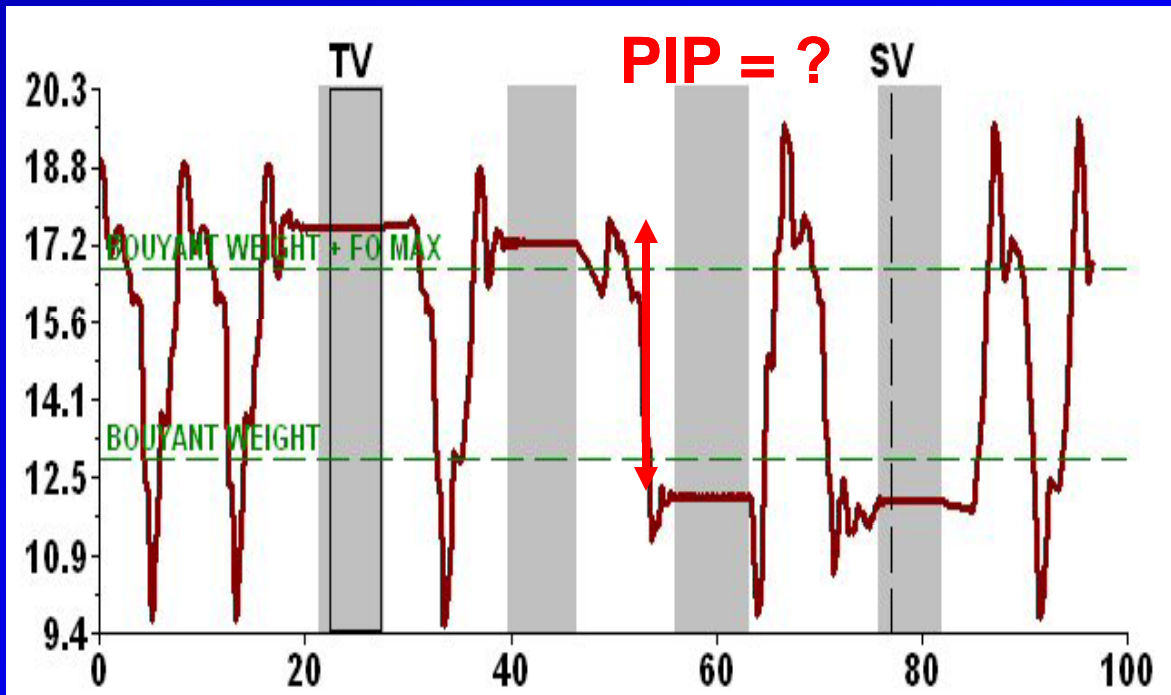
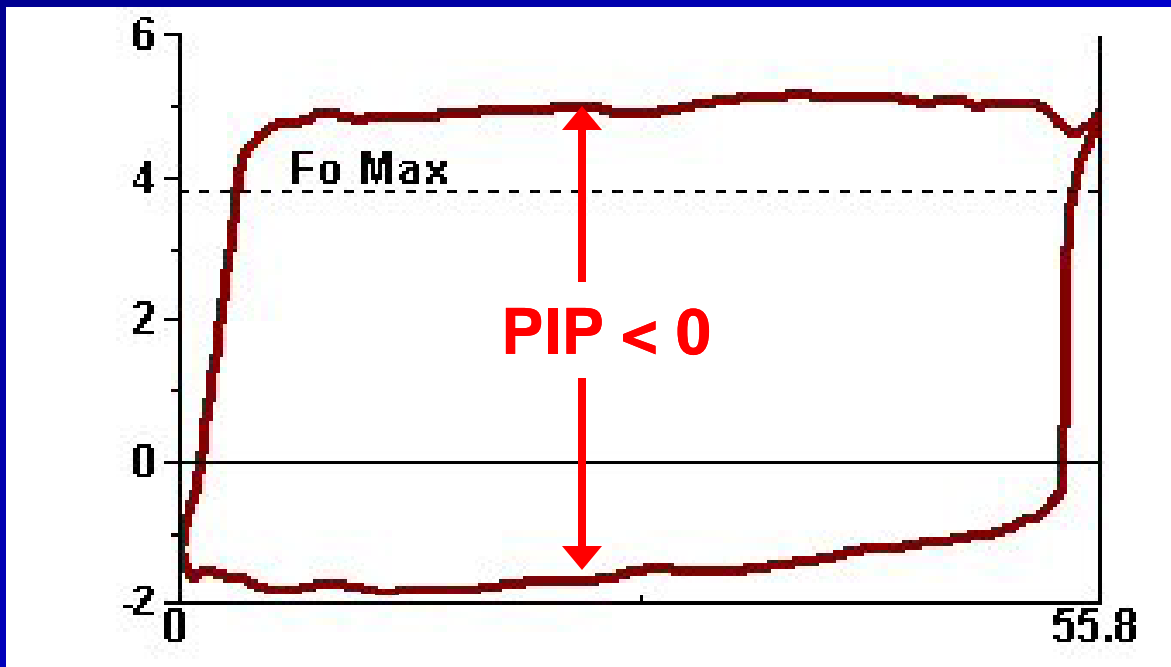
1. F_o can be calculated, where $F_o = (P_{dis} - P_{intk}) * A_p$, is the differential pressure acting on the cross-sectional area of the plunger [A_p]. Rod string picks up the fluid load acting on the traveling valve, plunger. The differential pressure, $(P_{dis} - P_{intk})$, is difference between the discharge pressure, [P_{dis}], and the intake pressure, [P_{intk}].
2. Solving for pump intake pressure: $(PIP = \text{Tubing Pressure} + \text{Pump Depth(TVD)} * \text{Fluid Gradient} - F_o / \text{Plunger Area})$ If you substitute in for F_o and set P_{intk} to zero, then you calculate F_{oMax} .
3. Pump intake pressure calculated from the Dynamometer card is usually less than the pump intake pressure determined from a fluid level. That is because the F_o , the height of the pump card is too high (not enough damping) and the $(P_{dis} - P_{intk})$ calculated is too high.

Unaccounted Wellbore Friction

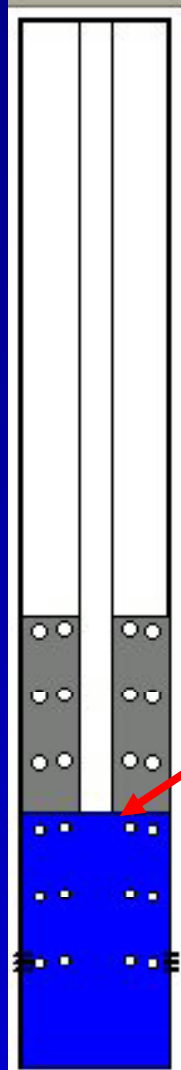


$Fo(fl) = 3505$
 $Fo(pc) = 3502$
 $Fo(vc) = 5518$

$\% \text{ Liq} = 27$
 $PIP = 268$

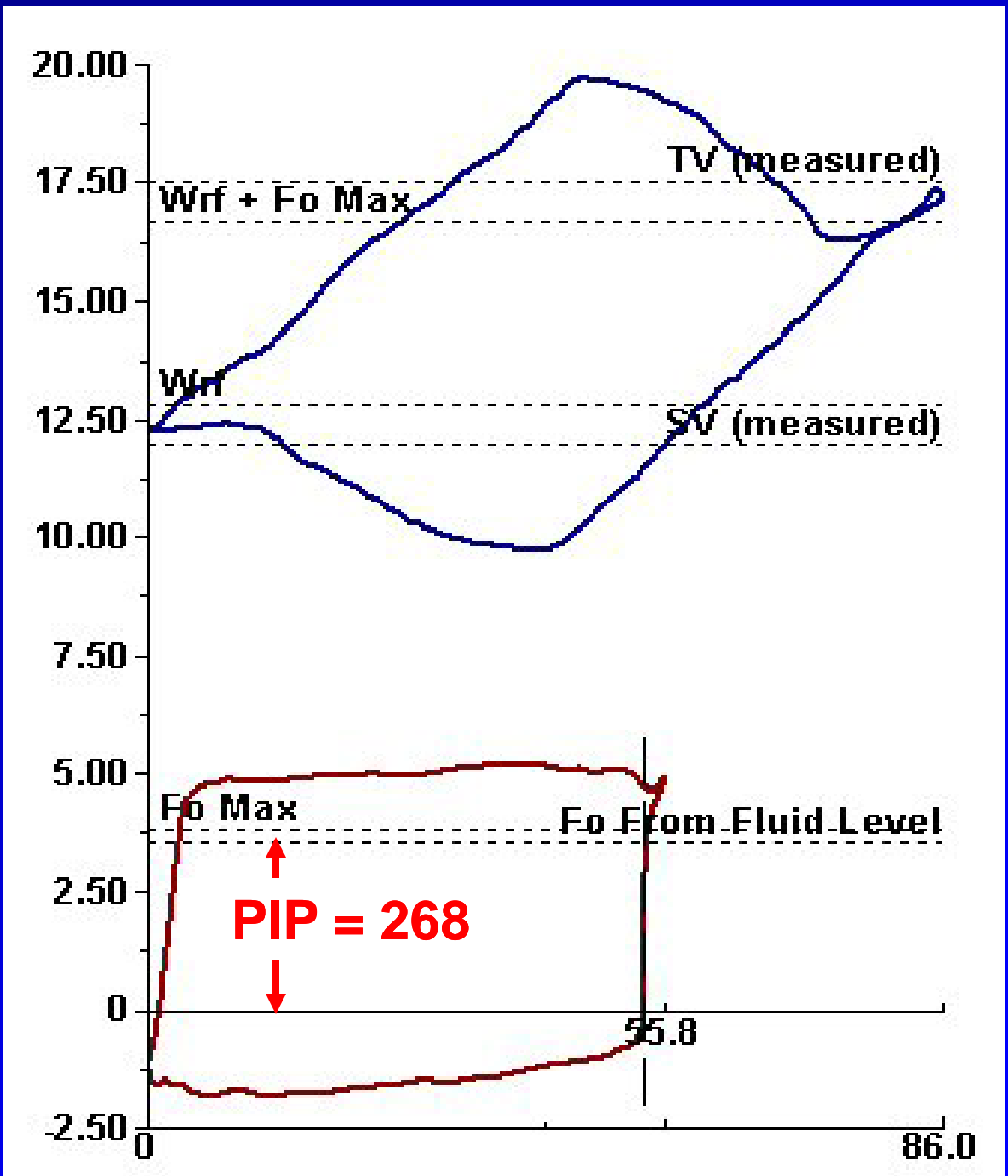


Unaccounted Wellbore Friction



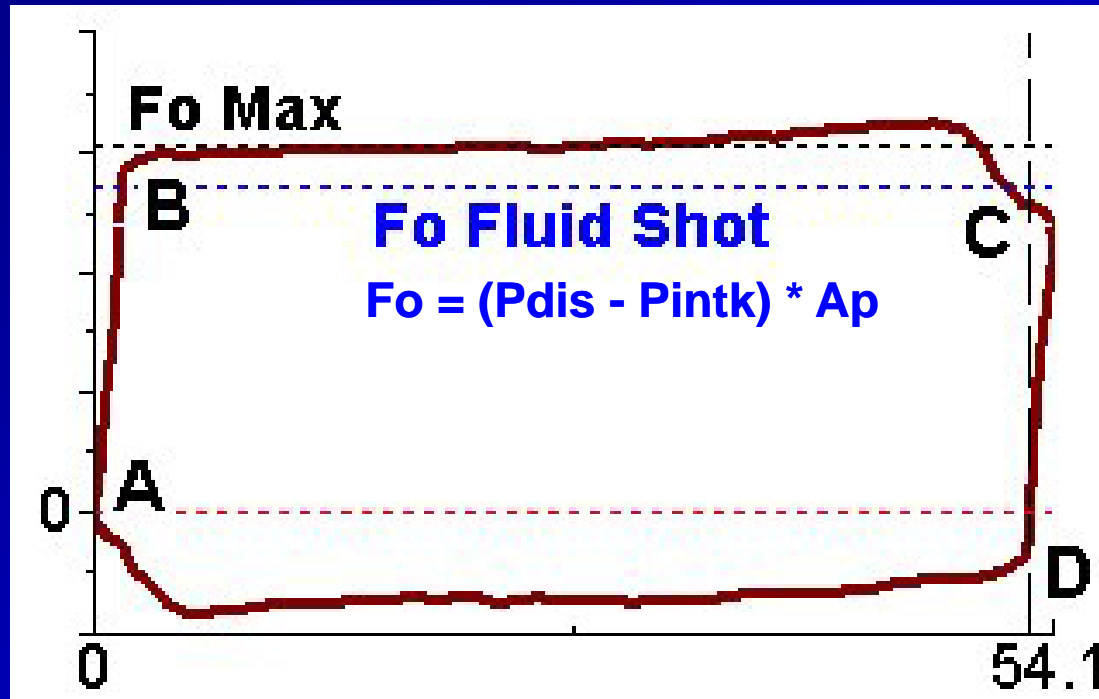
$Fo(fl) = 3505$
 $Fo(pc) = 3502$
 $Fo(vc) = 5518$

$\% \text{ Liq} = 27$
 $PIP = 268$



Excess Well Bore Friction:

Unaccounted Friction shows up in Pump Card



Possible Sources:

1. Paraffin
2. Scale
3. Over Tight Stuffing Box
4. Misalignment
5. Deviated Well
6. Pump Friction
7. Crimped Tubing
8. Other

Pump card has calculated loads much higher than the Fluid Load based on a shot Fluid Level. Pump card normally should set between the ZERO load line & Fo Max, pump loads outside this range indicate friction unaccounted for by wave equation.

Excess Well Bore Friction: Reduced Downhole Stroke & Raised Fluid Level

Select Liquid Level | Depth Determination | Casing Pressure BHP | Collars

Well State: Producing

Production	Current	Potential	Unit
Oil	3	3.5	BBL/D
Water	4	4.6	BBL/D
Gas	10	11.5	Mscf/D

IPR Method: Vogel

PBHP/SBHP: 0.30

Producing Efficiency: 86.8 %

Fluid Densities	Value	Unit
Oil	39	deg.API
Water	1.09	Sp.Gr.H2O
Gas Gravity	0.80	Air = 1

Acoustic Velocity: 1210.79 ft/s

Pump Intake Depth (MD): 7274.00 ft

Total Gaseous Liquid Column HT (TVD): 935 ft

Equivalent Gas Free Liquid HT (TVD): 935 ft

Comment:

Casing Pressure: 18.0 psi (g)

Casing Pressure Buildup: -0.0 psi

2.25 min

Gas/Liquid Interface Pres.: 23.8 psi (g)

Liquid Level MD: 6339.07 ft

Formation Depth MD: 7484.00 ft

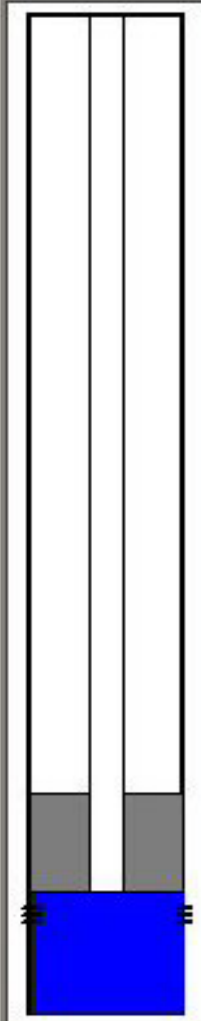
Annular Gas Flow: 0 Mscf/D

% Liquid: 100

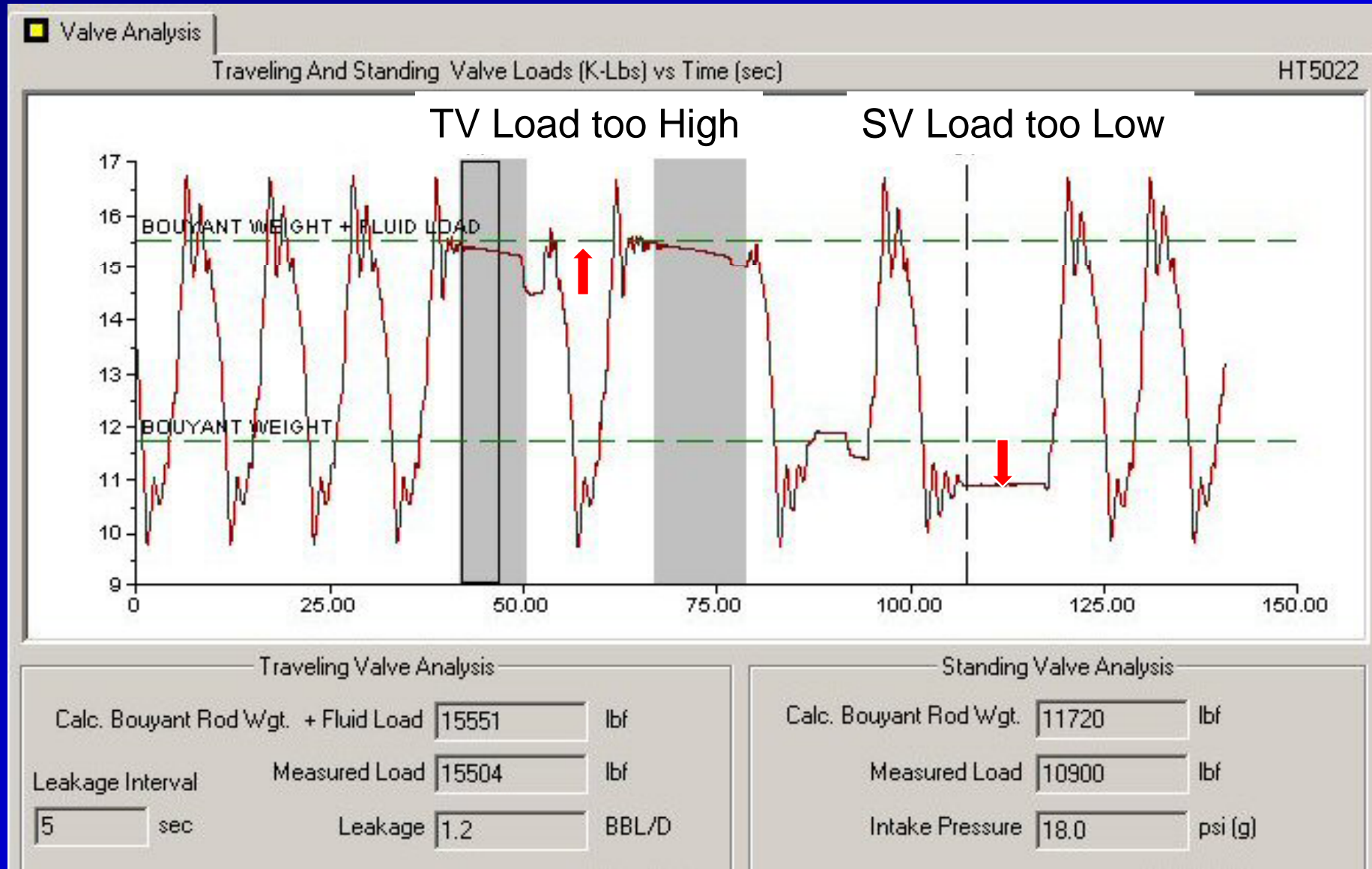
Pump Intake Pressure: 340.5 psi (g)

PBHP: 439.6 psi (g)

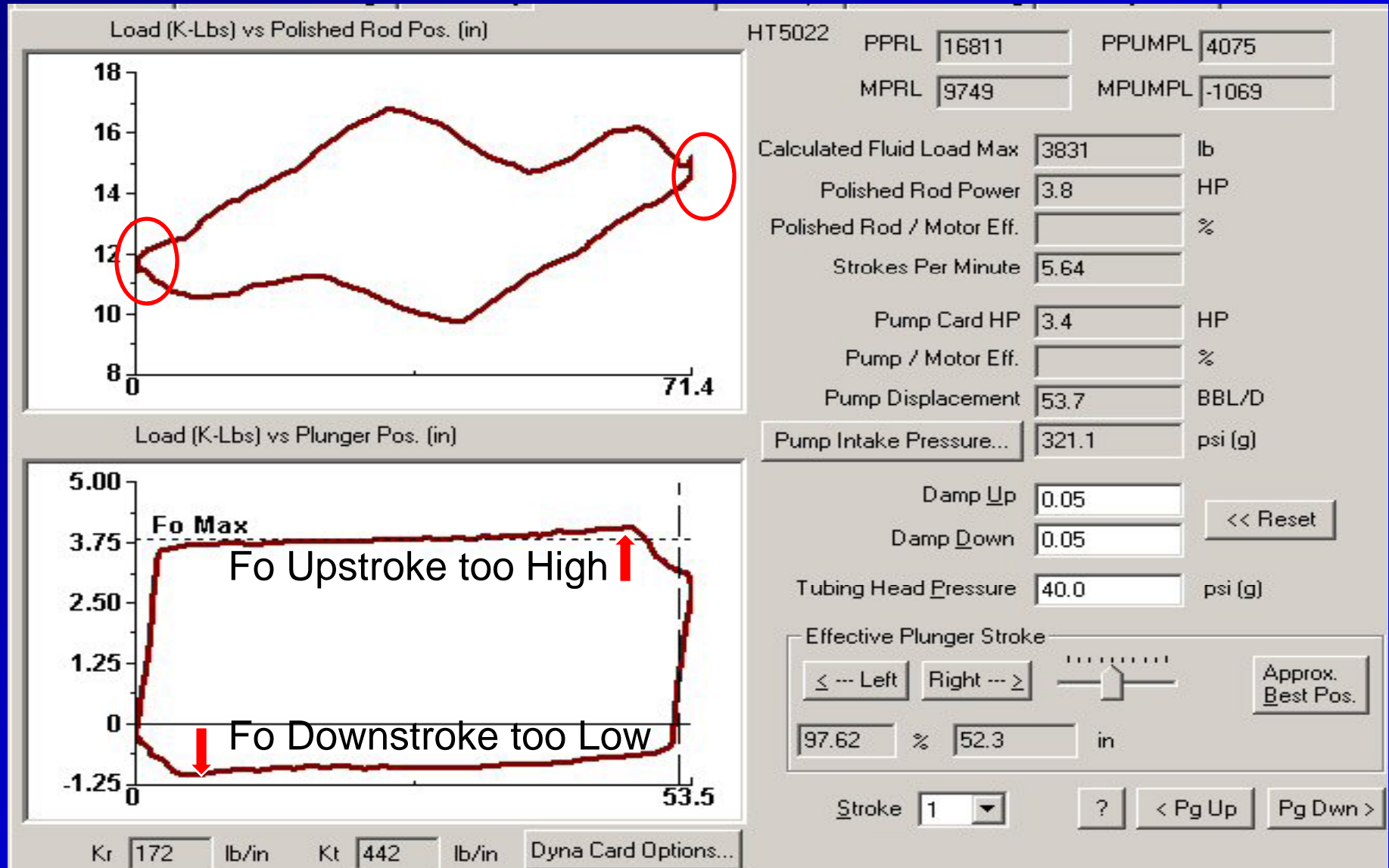
Reservoir Pressure (SBHP): 1500.0 psi (g)



Excess Well Bore Friction: Friction Affects Valve Load Test



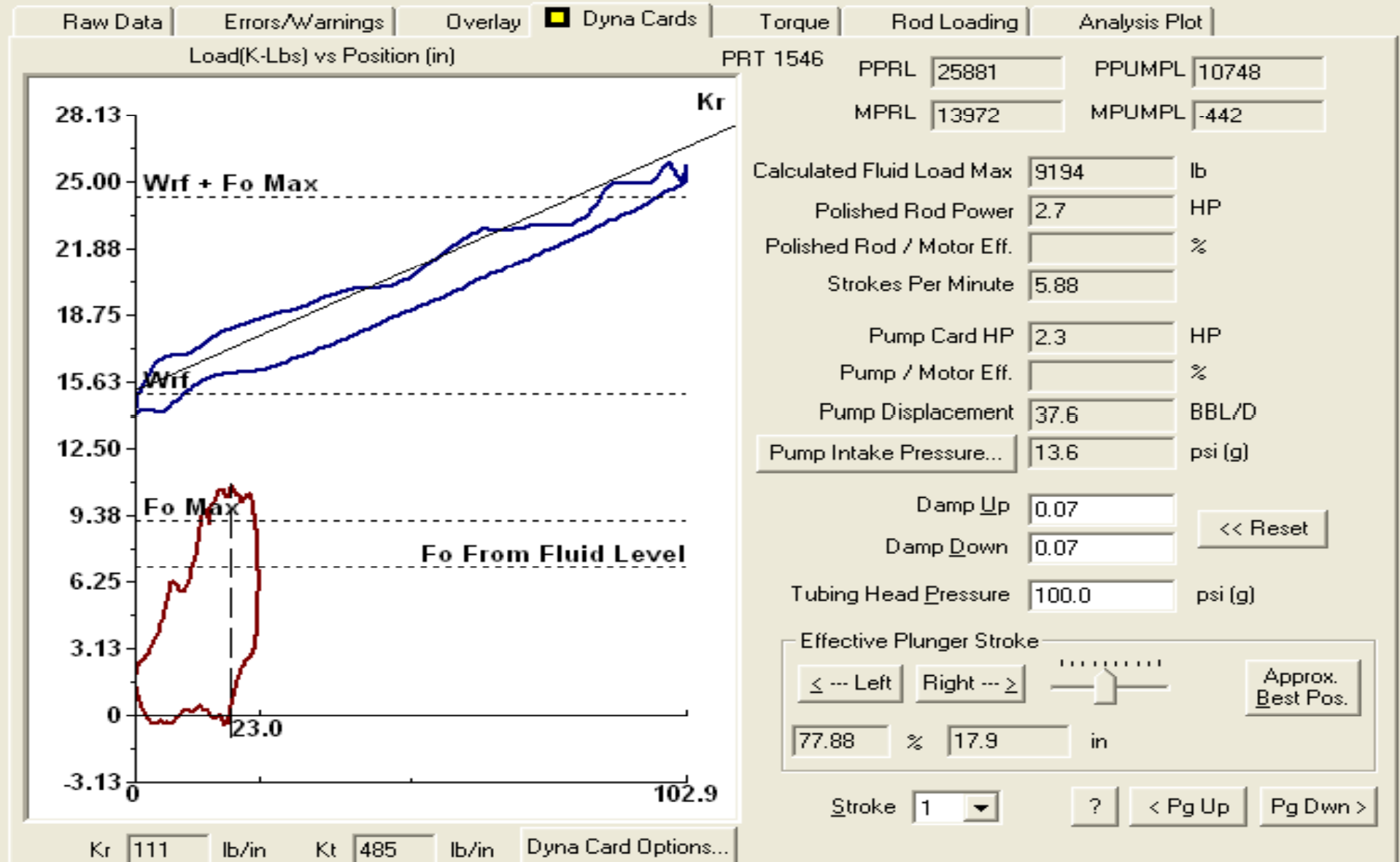
Excess Well Bore Friction: Friction Affects Dyno Cards



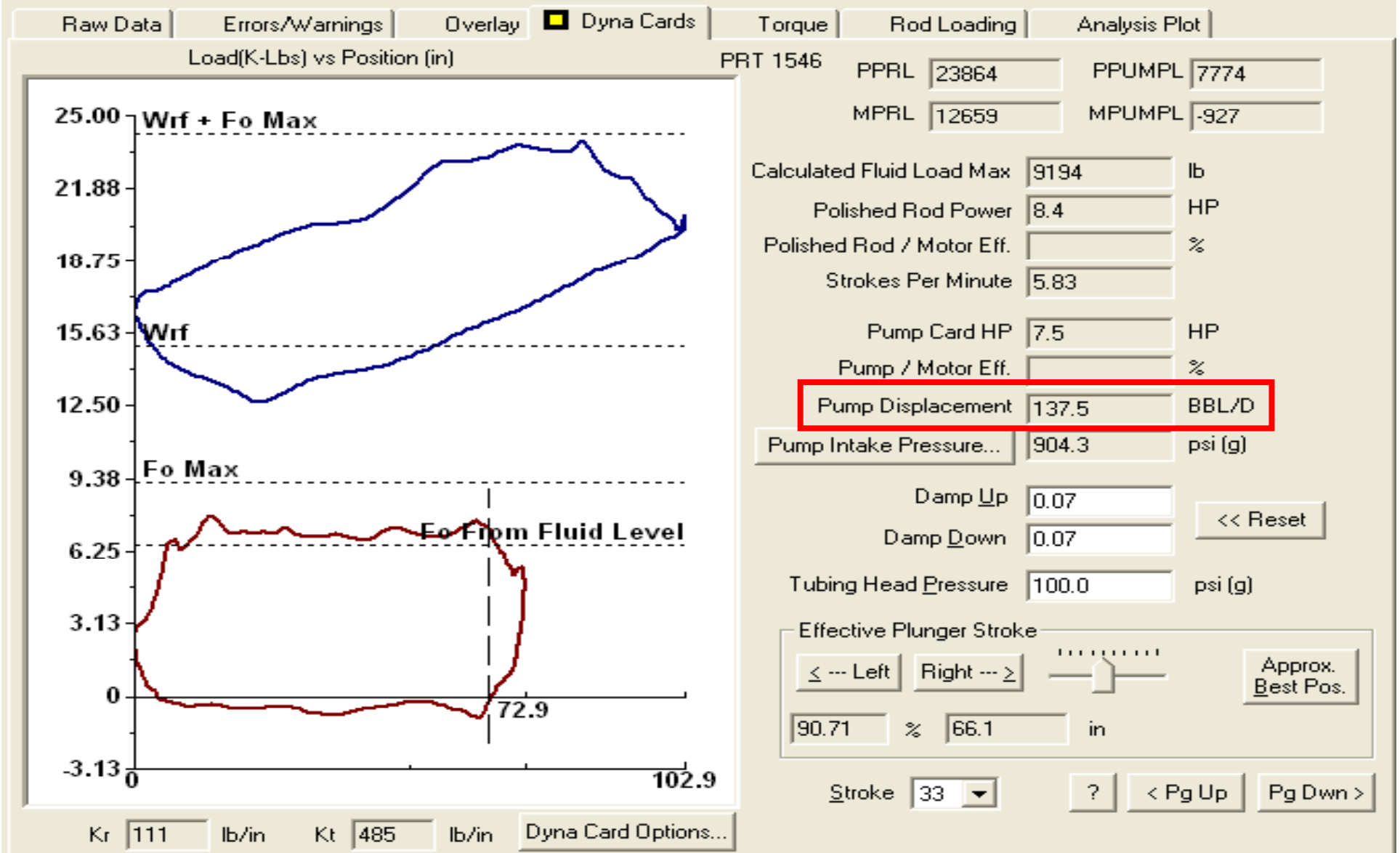
Excess Well Bore Friction Indicators

- 1) Fluid Level is higher than normal
- 2) Surface card shows a vertical change in load at the top and bottom of the stroke (Extra friction opposite to the direction of movement is broken by changing the direction of motion of the rod string)
- 3) Pump card should set between the ZERO load line & F_o Max, pump loads outside this range indicate of unaccounted friction.
- 4) SV valve check is low and TV check is too high (Friction is resisting the lifting the rods on the upstroke and friction is holding rod load on the downstroke)
- 5) TV load immediately drops as brake released (When the direction of motion changes or the rods go from stopped to moving the friction force that was being applied opposite to the prior motion of the rods is broken).
- 6) Low system efficiency

Investigation of Well Problem: 83% of Surface Stroke lost to Rod Stretch



After Hot Water Treatment +100 BPD



Adjusting Damping Coefficients

1. Iterative process used to estimate the proper damping coefficients
2. Note the position of the downhole dyno card when the damping coefficients are properly stated.
3. A finite amount of adjustment is further possible by fine tuning the specific gravity of the tubing fluid over the length of the rod string.
4. When the pump load lines B - C and D - A are nearly flat then the proper amount of damping has been added.
5. Concave out (like with 0.01) then need more damping.
6. Too much damping then lines B - C and D - A are concave in toward the center of the card and the damping coefficient are too high.
7. When the correct amount of damping is entered and the tubing pressure is entered, then the PIP from the pump card should be in good agreement with the PIP from the fluid level.
8. Some recommendations for default damping coefficients are approximately 0.01 per 1000 feet of well depth. For a well 3000' deep then 0.03 is a good initial guess for the value of damping.
9. Add 0.01 per 2000 feet for pump depths greater than 5000 feet.
10. **DO NOT HAVE TO CHANGE DAMPING**; just note that downhole friction is high and PIP from Pump Card too LOW!!!



File Mode Option Tools Help

- Acquire Mode
- Recall Mode

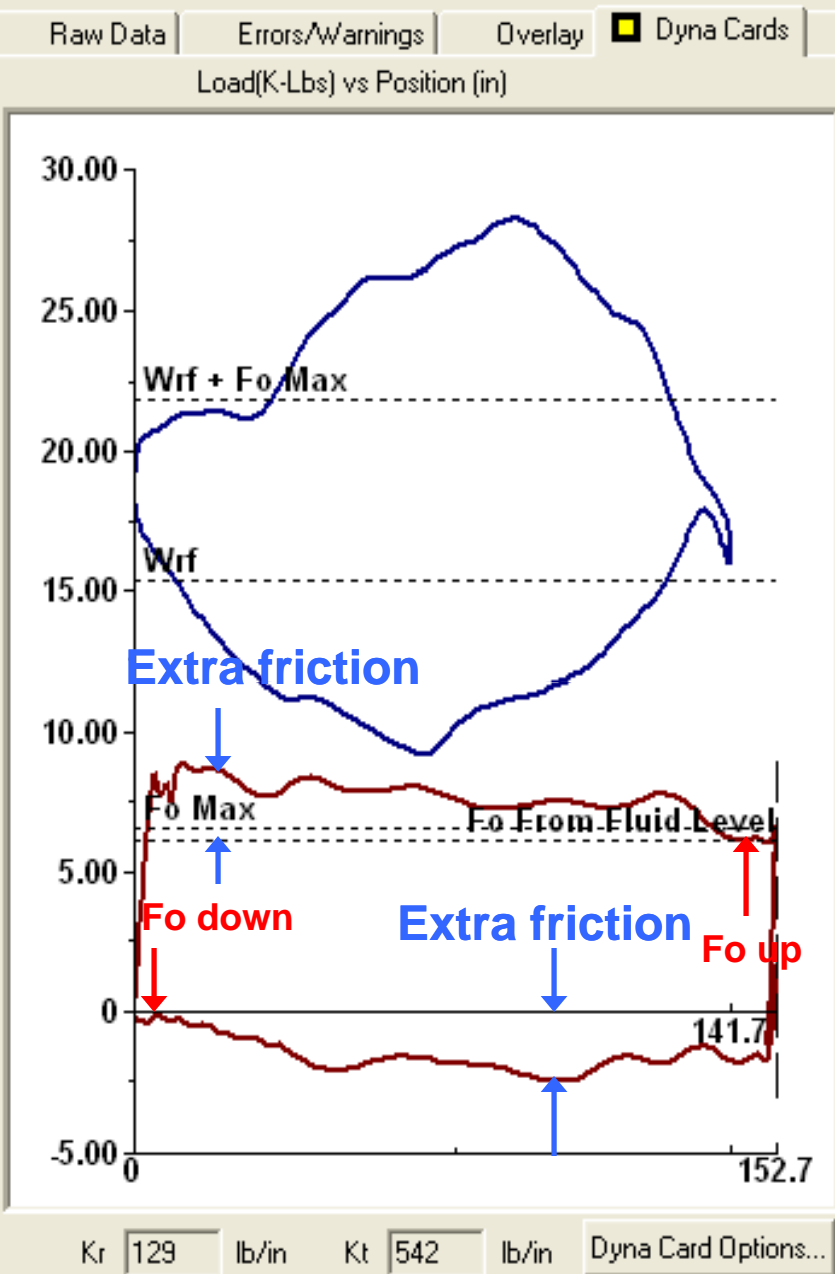
F2

Data Files

F3

Select Test

F4 Analyze



HT204 PPRL 28226 PPUMPL 8871
MPRL 9220 MPUMPL -2478

Calculated Fluid Load Max 6558 lb
Polished Rod Power 34.0 HP
Polished Rod / Motor Eff. %
Strokes Per Minute 8.22
Pump Card HP 28.8 HP
Pump / Motor Eff. %
Pump Displacement 329.2 BBL/D
Pump Intake Pressure... 72.4 psi (g)

Damp Up 0.05 << Reset
Damp Down 0.05

Tubing Head Pressure psi (g)

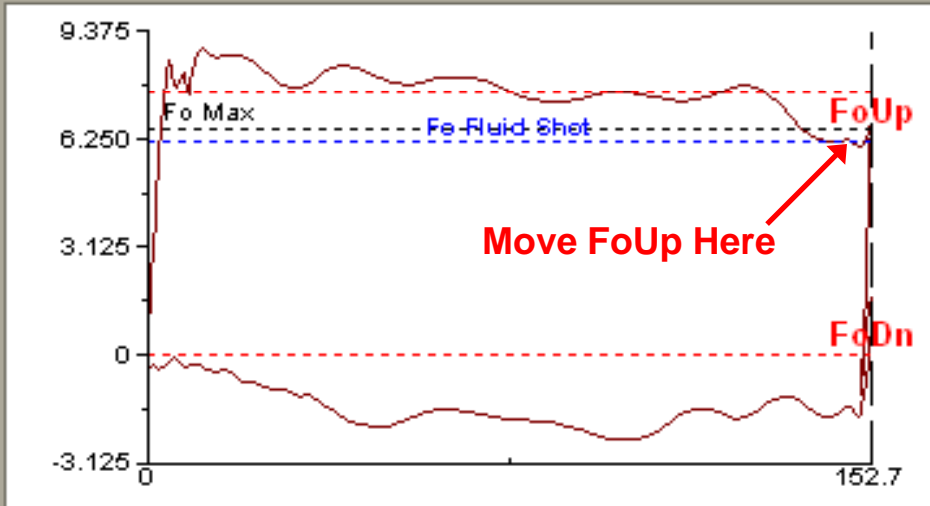
Effective Plunger Stroke

 100.00 % 152.7 in

Stroke 1 ? < Pg Up Pg Down >

Use Up Stroke Pump Load Option User Input to Move FoUp Line to the point shown below

Worksheet to Calculate Pump Intake Pressure using Fluid Load from Pump Card



Up Stroke Pump Load Options

- Average of Up Stroke Loads
- Maximum Up Stroke Load (adj. by Unaccounted Friction)
- Load at Pump Fillage Line
- User Input

Up Down

Fo Up 7617 lb

Down Stroke Pump Load Options

- Zero Load Line
- Minimum Down Stroke Load (adj. by Unaccounted Friction)
- Average of Down Stroke Loads
- User Input

Up Down

Fo Down 0 lb

Unaccounted Friction 2478 lb

Calculations For Fo (Fluid Load Plunger)

Fo Calculated From PIP of Fluid Level Analysis 6135 lb

Fo = Plunger Area * [Tbg Pres. - PIP + Pump Depth * Fluid Gradient]

Fo Calculated from Valve Check Analysis

Fo = (TV-SV)

Fo = FoUp - FoDown

Fluid Load (Fo) 7617 lb

PIP = Tubing Pressure + Pump Depth(TVD) * Fluid Gradient - Fo / Plunger Area

Pump Intake Pressure 72.4 psi

Include Worksheet In Reports

OK Cancel



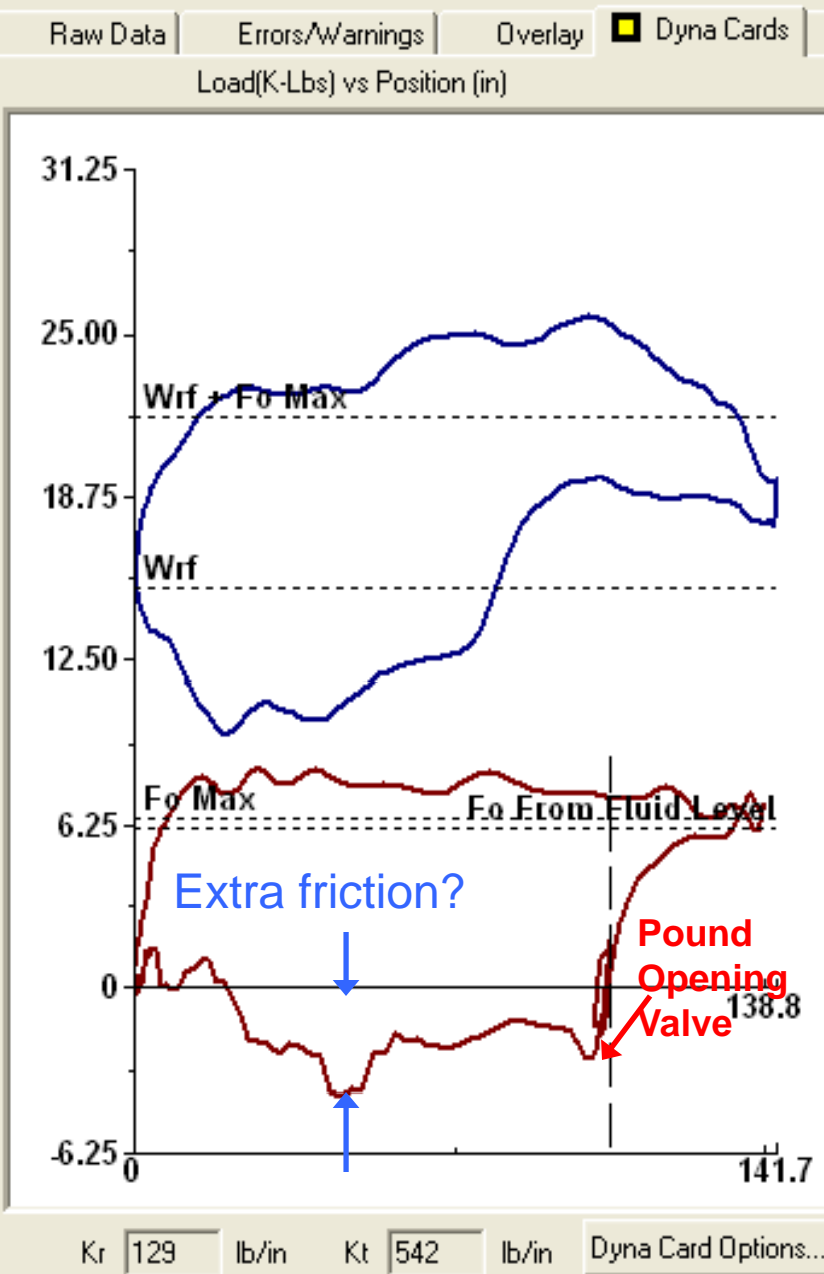
File Mode Option Tools Help

- Acquire Mode
- Recall Mode

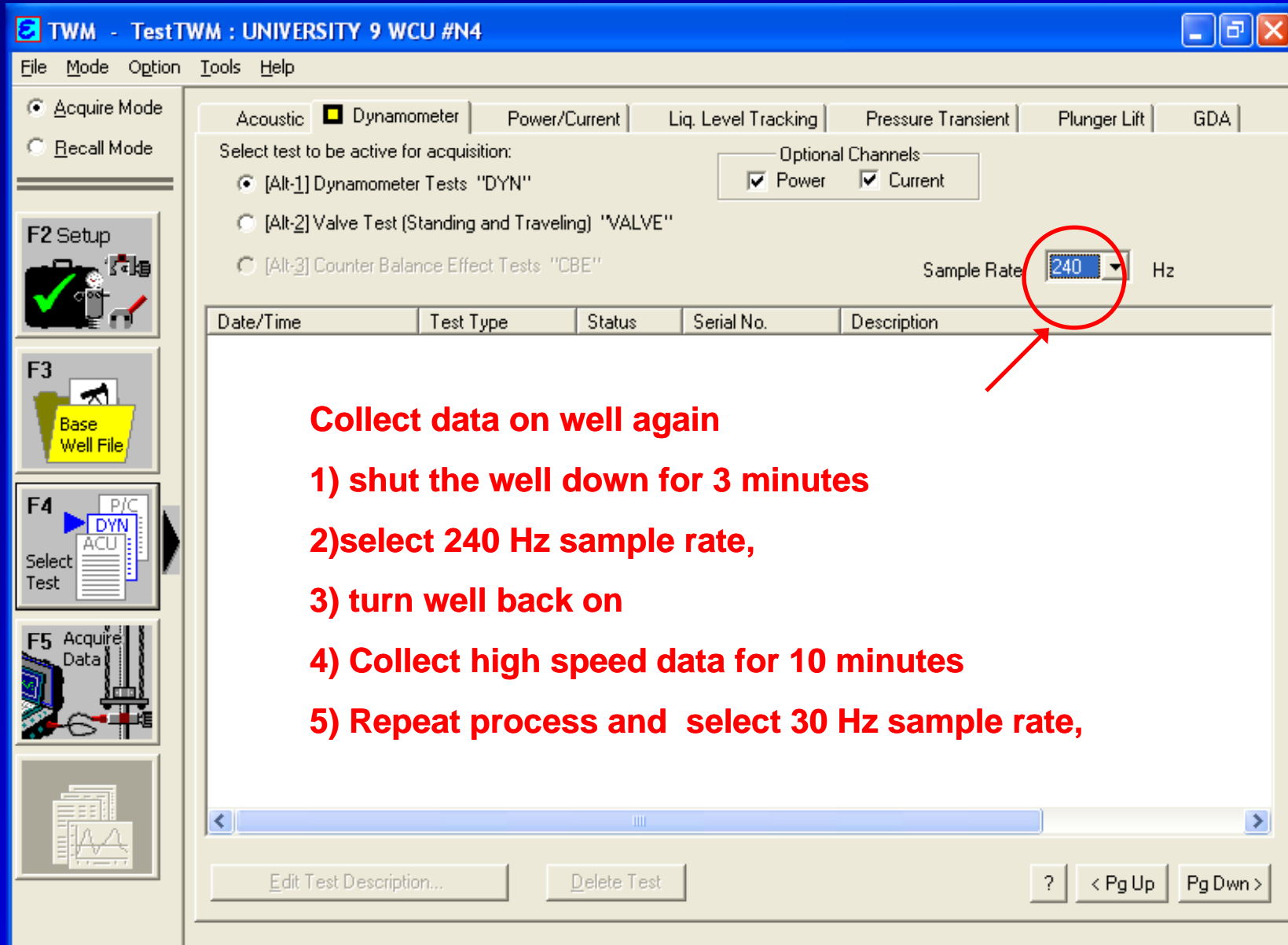
F2 Data Files

F3 Select Test

F4 Analyze



High speed sampling may help us understand what is happening on your well



Collect data on well again

- 1) shut the well down for 3 minutes**
- 2) select 240 Hz sample rate,**
- 3) turn well back on**
- 4) Collect high speed data for 10 minutes**
- 5) Repeat process and select 30 Hz sample rate,**

The screenshot shows the TWM software interface. The title bar reads 'TWM - TestTWM : UNIVERSITY 9 WCU #N4'. The menu bar includes 'File', 'Mode', 'Option', 'Tools', and 'Help'. On the left, there are function keys: 'F2 Setup', 'F3 Base Well File', 'F4 Select Test', and 'F5 Acquire Data'. The main window has tabs for 'Acoustic', 'Dynamometer', 'Power/Current', 'Liq. Level Tracking', 'Pressure Transient', 'Plunger Lift', and 'GDA'. The 'Dynamometer' tab is active. Below the tabs, there are radio buttons for test selection: '[Alt-1] Dynamometer Tests "DYN"', '[Alt-2] Valve Test (Standing and Traveling) "VALVE"', and '[Alt-3] Counter Balance Effect Tests "CBE"'. The 'DYN' option is selected. To the right, there are checkboxes for 'Optional Channels' with 'Power' and 'Current' checked. Below that, the 'Sample Rate' is set to '240' Hz. A table with columns 'Date/Time', 'Test Type', 'Status', 'Serial No.', and 'Description' is visible. At the bottom, there are buttons for 'Edit Test Description...', 'Delete Test', and navigation keys like '?', '< Pg Up', and 'Pg Dwn >'.

Damping

1. Unaccounted friction impacts shape of pump card; friction increases load range.
2. “Unaccounted” is extra friction not removed by the wave equation calculating pump card.
3. Damping coefficients subtract “friction” from rods as function of velocity.
4. 0.05 Default damping usually works OK.
5. Change TWM damping coefficients from the default to “Sort of” account for friction.
6. Wells having shallow depth with out much deviation; damping coefficients are usually 0.01/1000 foot depth. Use 0.01/2000’ for pump depths greater than 5000’.
7. Increase damping as the downhole fiction goes up or decrease damping as the well gets shallower.